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METHOD, COMPUTER PROGRAM AND OPEN AND/OR CLOSED-LOOP CONTROL  
UNIT FOR OPERATING AN ACTUATOR HAVING A CAPACITATIVE ELEMENT,  
AND INTERNAL COMBUSTION ENGINE

The present invention relates first of all to a method for  
operating an actuator having a capacitative element, an ohmic  
resistance being connected in parallel with the capacitative  
element and the value of the ohmic resistance being sensed at  
5 specific points in time.

Background Information

A method of the kind cited above is known from DE 199 58 406  
10 A1, which describes a piezoactuator that is used, for example,  
in a fuel injector. The piezoactuator behaves similarly to a  
capacitative element in electrical terms, and is therefore  
itself often referred to as a capacitative element. The  
capacitative element is longer or shorter depending on its  
15 charge state. The change in length of the capacitative element  
is transferred to a valve element of the fuel injector.

In the event of an interruption in activation of the  
capacitative element, or a malfunction of one of the  
20 components, it may happen that the capacitative positioner  
remains continuously in one specific position because it can  
no longer be discharged. In a context of use in a fuel  
injector, the result of this could be, for example, that the  
latter remains in the open position for a long period of time,  
25 and fuel is continuously injected into the combustion chamber  
of the internal combustion engine. This can result in severe  
damage to the internal combustion engine.

The ohmic resistance is provided to prevent such a situation. It enables discharging of the capacitative element even when the actual control line is interrupted, e.g. due to a cable break or a contact fault. The value of the ohmic resistance is dimensioned such that the time constant resulting from the capacitative element and the ohmic resistance is so great that no significant discharge of the capacitative element occurs within the usual activation time period that is usual for fault-free injection. On the other hand, the time constant is set in such a way that the capacitative element is sufficiently discharged within the maximum time available before the valve must definitely be closed in order not to damage the internal combustion engine.

DE 199 58 406 A1 proposes to sense the value of the ohmic resistance at specific points in time, and to draw conclusions therefrom as to the nature and/or the temperature of the capacitative element. The temperature dependence of the capacitative element can thereby be corrected.

It is the object of the present invention to enhance operating reliability when a capacitative element is used.

This object is achieved, in the context of a method of the kind cited initially, in that correct functioning of the ohmic resistance is monitored, and a fault signal is outputted upon detection of a malfunction.

#### Advantages of The Invention

The method according to the present invention monitors the functionality of the ohmic resistance representing a safety device. It is thus possible to detect states in which that safety device can no longer perform the function assigned to it. This in turn makes it possible, for example, to seek out

in timely fashion a maintenance facility that can repair the safety device, i.e. the ohmic resistance, and thus restore the operating reliability of, for example, an internal combustion engine.

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Advantageous refinements of the method according to the present invention are described in the dependent claims.

10 In a first refinement, it is proposed that the value of the ohmic resistance be sensed and be compared with a limit value. A corresponding method for sensing the value of the ohmic resistance is described in DE 199 58 406 A1, the disclosure of which is herewith expressly referred to. Sensing the value of the ohmic resistance and comparing the sensed value with a  
15 limit value is a very simple and reliable capability for checking the functionality of the ohmic resistance. This is because if the ohmic resistance loses contact with the capacitative element, e.g. as a result of a poor solder joint, the value of the ohmic resistance rises sharply. This can be  
20 unequivocally detected by way of the claimed comparison with a limit value. It is also possible to monitor whether the value of the ohmic resistance is within a tolerance band.

25 In a refinement thereof, it is proposed that the value of the ohmic resistance be sensed during a startup phase of a control unit with which the capacitative element is activated, and/or during a shutdown phase of the control unit when the latter is being switched off. The above-claimed sensing of the value of the ohmic resistance is not possible in every case during  
30 normal operation of the capacitative element. This is because in order to sense the value of the ohmic resistance (in accordance with the method indicated in DE 199 58 406 A1), it may be necessary to charge the capacitative element to a certain voltage and to sense the discharge curve through the  
35 ohmic resistance. A sufficiently high voltage is important in

this context, since the error becomes too great at excessively low voltages. This is not achievable during normal operation of the capacitative element.

5 Prior to actual operation of the capacitative element, however, there usually exists a startup phase of the control unit that activates the capacitative element. During this startup phase of the control unit, for example, a self-test is executed and certain initial values are set. The same also  
10 applies to the shutdown phase of the control unit, which is usually necessary for controlled shutoff of the capacitative element and of the device in which the capacitative element is being used. During these phases, the capacitative element is not yet being used as intended, so that charging and  
15 discharging for test purposes produce no interference here.

It is further proposed that the capacitative element be used in an injector of an internal combustion engine, and that the value of the ohmic resistance be sensed during a coasting mode  
20 of the internal combustion engine. No fuel is usually injected into the internal combustion engine while the internal combustion engine is in coasting mode. It is therefore appropriate to use this operating state in order to sense the value of the ohmic resistance.

25 In a particularly advantageous embodiment of the method according to the present invention, it is also proposed that correct functioning of the capacitative element be monitored. A corresponding method therefor is described in EP 1 138 905  
30 A1, the disclosure of which is likewise herewith expressly referred to. With this method according to the present invention, therefore, on the one hand correct functioning of the capacitative element is monitored, i.e. a determination is made as to whether activation from the control unit to the  
35 capacitative element is OK (cable break, loose connector,

etc.); and on the other hand, correct functioning of the ohmic resistance, i.e. the safety device of the capacitative element, is monitored. A very high level of safety is thus achieved with this refinement of the method according to the present invention.

In a refinement, it is proposed in this context that a first fault signal be outputted when it is determined that the ohmic resistance is working correctly and the capacitative element not correctly, or when it is determined that the capacitative element is working correctly and the ohmic resistance not correctly. The user of the capacitative element is, in this fashion, given concrete information regarding that specific malfunction. He or she can thus react accordingly, i.e. seek out a maintenance facility.

It is also proposed in this context that the capacitative element be used in an injector of an internal combustion engine; and that the first fault signal cause a reduction in the maximum permitted torque of the internal combustion engine. The internal combustion engine is thus shifted into a "safety mode" in which it can continue to be operated, but only in such a way that no permanent damage to the internal combustion engine occurs.

It is particularly preferred in this context that a second fault signal be outputted when it is determined that on the one hand the ohmic resistance and on the other hand the capacitative element are not working correctly. The result is to create a graduated fault message that informs the user not only of the existence of a malfunction, but also about the nature and severity of the malfunction. The user can thus react to the reported malfunctions in particularly effective and specific fashion. It is understood in this context that the second fault signal indicates a more serious malfunction

than the first fault signal. This is because if on the one hand the ohmic resistance and on the other hand the capacitative element are not working correctly, this means that the risk of damage to the apparatus being operated with the capacitative element is particularly high.

If the capacitative element is used in an injector of an internal combustion engine, the second fault signal should cause the affected cylinder to be shut off, the fuel pressure to be reduced, and/or the internal combustion engine to be shut down. These actions reduce the risk of permanent damage to the internal combustion engine, or in fact entirely rule out such a risk.

It is also advantageous if the first and/or the second fault signal result(s) in an input into a fault memory and/or the triggering of a specific alarm signal. This facilitates diagnosis at the maintenance facility and appropriate reaction by the user.

The present invention also relates to a computer program that is suitable for carrying out the aforesaid method when it is executed on a computer. It is particularly preferred in this context if it is stored on a memory, in particular on a flash memory.

The present invention further relates to an open- and/or closed-loop control unit for operating an internal combustion engine. It is particularly preferred in the context of such an open- and/or closed-loop control unit if it encompasses a memory on which a computer program of the aforesaid kind is stored.

Also the subject matter of the present invention is an internal combustion engine having a combustion chamber, having

at least one injector that encompasses a capacitative element as actuator and that encompasses an ohmic resistance connected in parallel with the latter. To enhance the operating reliability of the internal combustion engine, it is proposed that it encompass an open- and/or closed-loop control device of the aforesaid kind.

#### Drawings

An exemplary embodiment of the present invention is explained below in detail, referring to the appended drawings in which:

Figure 1 schematically depicts an internal combustion engine having an injector that encompasses a piezoactuator;

Figure 2 shows a detail of the piezoactuator of Figure 1 and a control unit for activating it;

Figure 3 is a flow chart of a method for operating the piezoactuator of Figure 1; and

Figure 4 is a flow chart of a further method for operating the piezoactuator of Figure 1.

#### Description of The Exemplary Embodiment

In Figure 1, an internal combustion bears in its entirety the reference character 10. It encompasses a combustion chamber 12 into which fresh air is introduced through an inlet valve 14 and an intake duct 16. The hot combustion gases are discharged from combustion chamber 12 through an outlet valve 18 and an exhaust duct 20.

Fuel is introduced directly into combustion chamber 12 through an injector 22 that is activated by a control unit 24 and

receives fuel under high pressure from a fuel system 26. Injector 22 encompasses a valve needle (not depicted in Figure 1) that is actuated by a piezoactuator 28. The fuel/air mixture present in combustion chamber 12 after an injection is ignited by a spark plug 30 (note in this context that the use of injector 22 is not confined to gasoline internal combustion engines, but that it can also be used in diesel internal combustion engines).

As is evident from Figure 2, piezoactuator 28 encompasses a multi-layer piezo positioner 32 whose length depends on its electrical charge state. Since a multi-layer piezo positioner of this kind has electrical properties similar to those of a capacitative element, it can also itself be referred to as a capacitative element. An ohmic resistance 34 is connected in parallel with multi-layer piezo positioner 32. Multi-layer piezo positioner 32 and ohmic resistance 34 thus constitute an RC element.

Piezoactuator 28 can be connected, for example via a hydraulic coupler (not depicted), to the valve needle of injector 22, and can influence the position of the valve needle depending on the voltage present at multi-layer piezo positioner 32. In an exemplified embodiment that is not depicted, the piezoactuator actuates a hydraulic control valve that causes a motion of the valve needle by way of a pressure change in a control chamber.

Multi-layer piezo positioner 32 and ohmic resistance 34 are, via their one terminal, on the one hand grounded (reference character 36) and on the other hand connected to an evaluation block 38 that is part of open- and closed-loop control unit 24 and is discussed in greater detail below. At their other terminal, multi-layer piezo positioner 32 and ohmic resistance 34 are on the one hand again connected to evaluation block 38



and on the other hand connected to an output stage switch 40. As once again discussed in detail below, the manner of connection of evaluation block 38 makes it possible to sense, by means thereof, the voltage drop occurring through RC element 32, 34.

Output stage switch 40 is activated by a control block 42 that receives and processes different input signals, also including signals from evaluation block 38. Multi-layer piezo positioner 32 and ohmic resistor 34 can be connected via output stage switch 40 to an energy source 44. Additionally disposed between output stage switch 40 and energy source 44 is a monitoring device 46 whose exact function will once again be discussed in detail below.

Control block 42 additionally activates a further output stage switch 48 that can ground (reference character 50) the other terminal of capacitative element 32 and of ohmic resistance 34. Piezoactuator 28 is connected to open- and closed-loop control unit 24 via a line 52 and a connector 54.

During normal operation of internal combustion engine 10, injector 22 with multi-layer piezo positioner 32 works as follows: When fuel is to be injected by injector 22 into combustion chamber 12 of internal combustion engine 10, first output stage switch 40 is closed by control block 42, and second output stage switch 48 is opened. Multi-layer piezo positioner 32 is thus connected to energy source 44. The voltage now present at capacitative element 32 causes an elongation of the capacitative element which, as already indicated above, causes valve needle of injector 22 to lift off from a corresponding valve seat and open a passage for fuel from fuel source 26 into combustion chamber 12.

When the injection of fuel into combustion chamber 12 is to be

terminated, output stage switch 48 is closed by control block 42 (output stage switch 40 having been opened again immediately after the end of the charging operation). Both terminals of multi-layer piezo positioner 32 are thus grounded (reference characters 36 and 50), so that multi-layer piezo positioner 32 discharges again and becomes correspondingly shorter. As a result, the valve needle of injector 22 once again comes into contact against the corresponding valve seat so that communication between fuel system 26 and combustion chamber 12 is again interrupted.

Reliable operation of capacitative element 32 is very important for the overall operating reliability of the internal combustion engine. Without corresponding countermeasures, it could happen that, for example in the event of a break in cable 52 or a loose connector 54, multi-layer piezo positioner 32 is no longer connected to open- and closed-loop control device 24 and thus can no longer be activated. If the connection between multi-layer piezo positioner 32 and open- and closed-loop control device 24 is interrupted while multi-layer piezo positioner 32 is charged, i.e. while an injection of fuel into combustion chamber 12 of internal combustion engine 10 is occurring, then without corresponding countermeasures, that injection might not be terminated. This could result in severe damage to internal combustion engine 10.

To prevent this, ohmic resistance 34 is connected in parallel with multi-layer piezo positioner 32. This resistance is dimensioned in such a way that the time constant resulting from multi-layer piezo positioner 32 and ohmic resistance 34 (which constitute an RC element) is so great that no significant discharge of capacitative element 32 occurs within the usual activation time period that is necessary and usual for a fault-free injection of fuel into combustion chamber 12.

On the other hand, the time constant is set so that multi-layer piezo positioner 32 is sufficiently discharged within the maximum time available before injector 22 must definitely be closed in order not to damage internal combustion engine 10. When appropriately dimensioned, ohmic resistor 34 therefore acts as a so-called "bleeder resistance."

If a break in line 52 or a detachment of connector 54 occurs while injector 22 is open, multi-layer piezo positioner 32 is therefore discharged through ohmic resistance 34, and injector 22 is thus closed again. Ohmic resistance 34 is therefore an important safety device of injector 22. The knowledge that this safety device is functional can thus enhance the overall operating reliability of internal combustion engine 10. The functionality of ohmic resistance 34 is determined, during a coasting mode of the internal combustion engine, during startup and during shutdown of open- and closed-loop control device 24, as follows (see Figure 3):

The method depicted in Figure 3 begins with a Start block 56. After this, in block 58 multi-layer piezo positioner 32 is charged to a defined voltage  $U$ . Simultaneously, a time counter  $t$  is set to zero. The subsequent query in block 60 checks whether the value of time counter  $t$  is greater than or equal to a time threshold  $t_1$ . If that is not the case, the time counter is then incremented in 62, and the query in block 60 is made again. If time counter  $t$  is greater than or equal to time threshold  $t_1$ , the voltage  $U_1$  at that time  $t_1$  is then measured in block 64.

The next step 66 queries whether the content of time counter  $t$  is greater than or equal to a second time threshold  $t_2$ . If that is not the case, the time counter is then incremented in block 68. If it is the case, the value  $U_2$  of the voltage at time  $t_2$  is then ascertained in block 70.

The voltage in the RC element constituted by multi-layer piezo positioner 32 and ohmic resistance 34 decreases over time according to an exponential function, the exponential function being determined substantially by a time constant. By measuring voltage U1 at time t1 and voltage U2 at time t2, it is possible to determine the time constant and, if the capacitance of capacitative element 32 is known, therefore the value R of ohmic resistance 34. This calculation of the value R is performed in block 72.

Block 74 then queries whether the value R is greater than a limit value G. If the response to the query in block 74 is No, this means that ohmic resistance 34 is working correctly (block 76). If, however, a solder joint with which ohmic resistance 34 is connected to multi-layer piezo positioner 32 is defective, for example, the value R of ohmic resistance 34 rises sharply and exceeds limit value G. In this case the response to the query in 74 is Yes, and that logical signal is further processed in block 78 in a manner depicted below in detail. The checking of the functionality of ohmic resistance 34 ends in an End block 80.

The method described above is also described in DE 199 58 406 A1, the disclosure of which is herewith expressly made part of the subject matter of the present Application.

Figure 4 depicts the processing in processing block 78 in detail. That processing contains substantially a combination of the logical Yes result of query block 74 with the logical results of the diagnosis of the functionality of capacitative element 32 by way of monitoring block 46 (see Figure 2). Block 82 queries whether multi-layer piezo positioner 32 is or is not functional. If a defect is present, a bit  $B_2 = 1$  is set at the output of block 82. If no defect is present, bit  $B_2 = 0$  is set at the output of block 82. Analogously, a bit  $B_1 = 1$  is set

at the output of query 74 if the value R of ohmic resistance 34 is greater than the limit value G, i.e. if there is a defect in ohmic resistance 34. The same bit  $B_1$  is set to zero when ohmic resistance 34 is working in fault-free fashion.

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The respective outputs of queries 74 and 82 are fed into three logical AND blocks 84, 86, and 88. The output of query block 74 is inverted in block 90 before being fed into block 84, and the output of query block 82 is inverted in block 92 before  
10 being fed into block 86. The two AND blocks 84 and 86 are connected on the output side to an OR element 94 whose output is again connected to an OR element 96. The output of AND block 88 leads directly to an OR element 98.

15 OR elements 96 and 98 ensure that the method described in Figure 4 is performed for all the cylinders 1 through i of internal combustion engine 10. The output of OR element 96 leads to an alarm block 100, and the output of OR element 98 to a second alarm block 102.

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If both bits  $B_1$  and  $B_2$  are equal to zero (capacitance element 32 and ohmic resistance 34 are each working correctly), a bit = 0 is also present at the respective outputs of AND blocks 84, 86, and 88, so that ultimately neither alarm block 100 nor  
25 alarm block 102 is activated. If, however, bit  $B_1 = 1$  (ohmic resistance 34 is defective), and bit  $B_2 = 0$  (capacitance element 32 is working correctly), this results in a bit = 1 at the output of AND block 86, so that ultimately alarm block 100 is activated.

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The same also applies to the case in which bit  $B_1 = 0$  (ohmic resistance 34 is working correctly), but bit  $B_2 = 1$  (capacitance element 32 is defective). In this case a logical value of 1 is present at the output of AND block 84, once  
35 again ultimately resulting, via OR element 94, in the

activation of alarm block 100. Lastly, if bit  $B_1 = 1$  (ohmic resistance 34 is defective) and bit  $B_2 = 1$  (capacitative element 32 is defective), this then results in a bit = 1 at the output of AND block 88, which ultimately causes the  
5 activation of alarm block 102.

Alarm block 100 causes an input into a fault memory and the illumination of a warning light. In addition, the maximum torque that can be generated by internal combustion engine 10  
10 is reduced. Upon activation of alarm block 102, on the other hand, the affected cylinder is shut down, fuel pressure is reduced and, if applicable, the entire internal combustion engine 10 is shut down. The method depicted in Figure 4 thus permits a graduated reaction, depending on whether only piezo  
15 positioner 32 or only ohmic resistance 34, or both piezo positioner 32 and ohmic resistance 34 simultaneously, are defective.